

2

POR-2239(EX)
(WT-2239)(EX)
EXTRACTED VERSION

OPERATION SUN BEAM, SHOT SMALL BOY

Project Officer's Report—Project 7.1.4

Transient Radiation Effects Measurements on Guidance
System Circuits

P. J. Sykes, Jr., Project Officer
Air Force Systems Command
Kirtland AFB, NM

20 April 1964

DTIC
ELECTE
FEB 27 1986
S D D

NOTICE:

This is an extract of POR-2239 (WT-2239), Operation SUN BEAM, Shot Small Boy,
Project 7.1.4.

Approved for public release;
distribution is unlimited.

Extracted version prepared for
Director
DEFENSE NUCLEAR AGENCY
Washington, DC 20305-1000

1 September 1985

AD-A995 378

DTIC FILE COPY

06 2 20 008

OPERATION SUN BEAM

SHOT SMALL BOY

PROJECT OFFICERS REPORT — PROJECT 7.1.4

TRANSIENT RADIATION EFFECTS MEASUREMENTS
ON GUIDANCE SYSTEM CIRCUITS

Paul J. Sykes, Jr., T/Sgt, USAF
Project Officer

Research Directorate
Air Force Special Weapons Center
Air Force Systems Command
Kirtland Air Force Base
New Mexico

This document is the author(s) report to the Chief, Defense Atomic Support Agency, of the results of experimentation sponsored by that agency during nuclear weapons effects testing. The results and findings in this report are those of the author(s) and not necessarily those of the DOD. Accordingly, reference to this material must credit the author(s). This report is the property of the Department of Defense and, as such, may be reclassified or withdrawn from circulation as appropriate by the Defense Atomic Support Agency.

DEPARTMENT OF DEFENSE
WASHINGTON 25, D. C.

Accession For	
NTIS CRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By	
Distribution/	
Availability Codes	
Dist	Avail and/or Special
A-1	

UNANNOUNCED



1.4 DESIGN OF EXPERIMENT

Assuming a (fission) device detonated 10 feet above ground, circuit test locations were selected for dose rates of approximately However, Small Boy was later changed, after the instrumentation pads were installed, to a device of approximately yield. New estimates of the nuclear environment predicted at the station locations were obtained from Major Byron H. Shields, Program 7 Director, and were based on Los Alamos Scientific Laboratory (LASL) predictions for the device as calculated by the Biophysics Division of the Research Directorate, AFSWC.

The burst was treated as a surface detonation for both blast and thermal calculations, since the burst was only ten feet above ground level. In Reference 1 it was estimated that the total thermal radiation could be calculated from the following equation:

$$Q = \frac{2.6 \times 10^{11} \text{ Cal/kt} \times \text{yield in kt}}{1.168 \times 10^4 \text{ cm}^2/\text{ft}^2 \times R^2} \quad (1.1)$$

$$Q =$$

Where: Q = thermal exposure, cal/sec

The times of air shock arrival and peak overpressure versus distance were derived by Sachs scaling of the surface burst curves given in Reference 2 to a yield of and to an altitude of 4200 feet (NASA standard atmosphere).

Estimates of the electric and magnetic fields used in subsequent calculations in this Chapter are taken from Reference 3.

For a nuclear weapon, the radius of the ionized region, a , producing the electromagnetic pulse was estimated from the relation

$$W = 4.55 \times 10^{-5} a \exp \left\{ 25 \left[1 - \exp (-0.1254a) \right] \right\} \quad (1.2)$$

Where: W = yield Mt

a = effective radius, kilometers.

For the Small Boy event, a was approximately feet. At distances less than it was expected that there might be large electric fields of sufficient size to produce electrical breakdown in the ionized air. The electric fields for distances outside this region were estimated from the following equations:

$$E_{\max} = \frac{3000 a}{R} \left[1 - \frac{(a)^2}{R} + \frac{(a)^4}{R} \right]^{\frac{1}{2}} \quad (1.3)$$

Where:

- E_{\max} = peak electric field, volts/meter
- a = effective radius, feet
- R = distance, feet

Low-frequency magnetic fields could not be predicted reliably. The maximum value for the high-frequency horizontal component was estimated from the equation:

$$H_{\phi} = \left[\frac{100 W}{R^2} \exp. (-2.5R) \right]^{0.43} \quad (1.4)$$

Where:

- H_{ϕ} = horizontal component, oersteds
- R = distance, kilometers
- W = yield, Mt

The maximum rate of change of the magnetic field was estimated from the relationship:

$$\frac{dH_{\max}}{dt} = 10^6 H_{\max} \quad (1.5)$$

Where:

- H_{\max} = magnetic field
- t = time, seconds

Fallout doses were estimated using TM-23-200 (Reference 4). The ground shock parameters were taken from Brode's report (Reference 5) on protective construction.

Table 1.1 summarizes the predicted environment at each station location.

The blooper and diagnostic stations on this equipment were designed to reduce all associated weapon environments such as thermal, blast and EMP, to below damage-threshold levels for the circuits and instrumentation involved.

Thin aluminum fallout covers were installed at each pad to minimize contamination of the package between H-hour and recovery time. Each diagnostic and blooper package was placed in a 1/4-inch-thick steel box to prevent damage from blast and over-

TABLE 3.2 GENERAL SHOT DATA, SHOT -MALL BOY

Device	
Yield	
Date	14 July 1962
Time of detonation	11:30 00.123 PDT
Burst Medium	Air
Actual Height of Burst	10 feet
Placement	Wooden Tower
Nevada State Coordinates	N 747,907.43 E 717,118.39
Surface Zero	Ground
Air Pressure at Surface GZ(Hg)	26.67
Air Pressure at Surface GZ(Mb)	904
Air Temperature ($^{\circ}$ C)	31.7
Relative Humidity (%)	16
Dew point ($^{\circ}$ C)	2.8
Surface wind direction/Velocity ₀ /Mph	225/06

REFERENCES

1. R. W. Hillendahl; "Characteristics of the Thermal Radiation from Nuclear Detonations"; AFSWP 902, 30 June 1959; U. S. Naval Radiological Defense Laboratory, San Francisco, California; Secret Restricted Data.
2. James F. Moulton, Jr.; "Nuclear Weapons Blast Phenomena"; DASA-1200, March 1960; U. S. Naval Ordnance Laboratory, White Oak, Maryland; Secret Restricted Data.
3. Conclusions and Recommendations of the Ad Hoc Panel of EM Radiation. STL Report 6101-6055-GQ000, 28 December 1961; Space Technology Laboratories, Inc., Redondo Beach, California; Secret Restricted Data.
4. "Capabilities of Atomic Weapons"; Department of the Army Technical Manual TM 23-200, Department of the Navy OPNAV Instruction 03400.1B, Department of the Air Force AFL 136-1, Marine Corps Publications NAVMC 1104 Rev; Revised Edition, November 1957; Prepared by Armed Forces Special Weapons Project, Washington, D. C.; Confidential.
5. "Weapons Effects for Protective Designs—Ground Support System Weapon Effects"; RC Report P-1951, March 1960; The RAND Corporation, Santa Monica, California; Unclassified.
6. "Transient Radiation Effects Tests"; Final Report PX 2643, 1 January 1963; UNIVAC Division of Sperry Rand Corporation, 4th Ave. and 23d Street, New York; Secret Restricted Data.
7. "Final Report on Small Boy Project for Northrop Ventura"; IBM Report 62-521-9, 2 May 1962; IBM Corporation, New York; Unclassified.
8. Montgomery Phister; "Logical Design of Digital Computers"; 1958; McGraw-Hill Publishing Company, Inc., New York; Unclassified.
9. Personal Correspondence with R. S. Caldwell; The Boeing Co., Seattle, Washington.
10. Boeing Internal Report 2-5471-5-94 (revised), dated 17 October 1962; The Boeing Company, Seattle, Washington.
11. Hughes Aircraft Co. Report FR 63-17-32, "Transient Radiation Effects on Missile Electronic Circuits"; Hughes Aircraft Company, Fullerton, California.
12. P. Gianas, Kearfott Division, General Precision Equipment, Inc., 90 Gold Street, New York; Letter to: Capt K. Gilbert, Ballistic Systems Division, Air Force Systems Command, AF Unit P. O., Los Angeles 45, California; 29 May 1962.
13. Personal Communication with J. E. Bell, Hughes Aircraft Company, Fullerton, California.
14. Boeing Presentation at 7 and 8 November 1962 Small Boy TREE Working Group Meeting at Aerospace Corporation, El Segundo, California.
15. Personal Communication with H. W. Wicklein, The Boeing Company, Seattle, Washington.